

Chapter 20

An Approach to Develop Hansel–Spittel Constitutive Equation during Ingot Breakdown Operation of Low Alloy Steels

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- DOI: 10.1007/978-981-10-4819-7_20

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Abstract

The control of the final quality of a forged product requires an in-depth comprehension of quality of the initial cast ingot. Hot workability is an important property which can be evaluated by variation of strain, strain rate, and temperature. Modeling of forging process always needs to define constitutive models for the material involved. In this study, 42CrMo steel with dendritic microstructure was used to generate the flow stress curves. In order to provide accurate predictions of the thermal and mechanical parameters in the actual ingot breakdown operation, hot compression tests were carried out at uniform temperatures ranging from 1050°C to 1200°C and strain rates from 0.25s⁻¹ to 2s⁻¹. Finally, Hansel-Spittel law was developed to represent the dependency of the material flow stress on strain, strain rate and temperature. FE Simulation results reveal that the model is able to predict the adiabatic heating during deformation.

Introduction

Hot workability is an important property to estimate materials plastic deformation ability, which is usually defined as the amount of deformation that a material can undergo without cracking and reach desirable mechanical properties and microstructure at a given temperature and strain rate is generally evaluated by various parameters like strain rate, strain and temperature. Forging of ingot after casting starts with ingot breakdown process which is generally performed at very high temperatures (0.75 of melting point " M_P ") so as to breakdown the chemical (macrosegregation) and microstructural structure (as-cast dendritic) inhomogeneity [1]. Flow characteristic of a hot forging process consists of strain hardening and softening due to dynamic processes like recrystallization and recovery, which basically determines the quality of a forging product. Constitutive relations are often used to model the forging process in order to describe the plastic flow properties of metals and alloys, many research groups have attempted to develop constitutive equations using various models to describe the flow behavior of various alloys using experimental data [2-5]. Despite large efforts

being made on the development of constitutive equations for 42CrMo, further investigation has to be done describing the behaviour of 42CrMo in its as-cast structure at very high temperatures ($\sim 0.7\text{Mp}$) so as to describe the flow behavior during the ingot breakdown process. Therefore the objective of this study is to investigate the nature of the influence of strain rate and temperature on compressive deformation characteristics of 42CrMo using hot compressive tests. A model describing the relationship of flow stress, strain rate, strain and temperature is proposed and used to simulate real time analysis of the process using Forge NxT 1.0[®] software.

Experimental

As- cast 42CrMo high strength steel was used for the present investigation. The composition of the alloy is shown in Table1. The materials were provided by Finkl Steel Co., Sorel Tracy, Quebec, Canada. Cylindrical specimens were machined with a diameter of 10mm and a height of 15mm. Hot compression tests were performed in Gleeble 3800 Thermomechanical Simulator at four different temperatures (1050, 1100, 1150 and 1200°C) and four strain rates (0.25, 0.5, 1 and 2s^{-1}). The heating rate was $2^\circ\text{C}/\text{Sec}$ till 1260°C where it was maintained for 300sec so as to get homogenous temperature over the specimen. The specimen was then cooled to a respective deformation temperature at a cooling rate of $1^\circ\text{C}/\text{Sec}$.

Table 1: Composition of as-cast 42CrMo (Wt.%)

C	Mn	Si	Mo	Cr	Ni	Other
0.35	0.85	0.40	0.45	1.85	Added	Microalloying

Results

For the present report, results from a deformation temperature of 1200°C and 1150°C at strain rates of 0.25s^{-1} and 2s^{-1} are considered. Stress- strain curve of hot compression tests (Fig. 1) reveals that at low strain rates, dynamic softening mechanisms get activated and results in stress drop after a peak stress. This is a typical recrystallization curve, which comprises of four states: the work hardening state, transition state, softening state and steady state. At high strain rates, the flow curves rises sharply and then attains a steady state. This type of flow curve resembles to that of recovery behavior due to which the flow stress attains a steady state due to dislocation generation and annihilation process running simultaneously. Dislocations are particularly needed to build a reservoir of stored energy. This stored energy along with the thermal energy is useful breaking down the coarse grains and generating much finer recrystallized grains. High temperatures can provide sufficient driving force along with dissolution of precipitates can lead to dislocation annihilation and thus softening can be seen as in Fig.1 at strain rate of 0.25s^{-1} . However, higher strain rates do not show softening even at

high temperatures due to the fact that critical driving force has not reached because of high Zener Hollomon factor, Z [6]. Low strain rates promote sufficient driving force for the dislocation annihilation and thus softening can be seen in Fig 1(a).

Constitutive Equation of the flow stress

To investigate the deformation behavior of as-cast 42CrMo steel, there is a need to develop constitutive equations in order to simulate the process of the ingot breakdown process. Material constants of the constitutive equation can be derived from the stress strain data obtained from the hot compression tests. To simulate bulk metal forming, Forge NxT 1.0[®] software is used which generally uses thermo- viscoplastic constitutive models under hot conditions. One of the most used models for bulk forming is Hansel-Spittel model. It is based on simple relation on three variables like strain, strain rate and temperature. It has been used for various alloys like AZ31 magnesium alloy [7] , 20MoCrS4 [8], Al-0.7%Mg-0.4%Si aluminum alloy [9], AA6082 alloy [10]. The model was developed by Hansel and Spittel, commonly termed as HS equation [11] is given as:

$$\sigma = Ae^{m_1 T} \varepsilon^{m_2} \dot{\varepsilon}^{m_3} e^{\frac{m_4}{\varepsilon}} (1 + \varepsilon)^{m_5 T} e^{m_7 \varepsilon} \dot{\varepsilon}^{T m_8} T^{m_9} \quad (1)$$

where, σ = Stress, ε = Strain, $\dot{\varepsilon}$ = Strain Rate, T = Deformation Temperature, m_1 to m_9 define the material's sensitivity to temperature, m_5 defines coupling temperature and strain, m_8 term coupling temperature and strain rate, m_2 , m_4 and m_7 define the material's sensitivity to strain and m_3 depends on the material's sensitivity to strain rate. Usually constants m_8 and m_9 are taken as zero. The material constants were calculated using linear regression methods by Origin[®] software and are provided in Table 2. The constants were then applied in the equation for various values of strain, strain rate and temperature in order to find the values of stress. Fig. 1 shows the comparison between experiment and calculated flow stress curves developed by constitutive equations. The Hensel- Spittel model is able to describe the steady state phase of hot flow stress curves at high strain rate, whereas it was not able to take into account the softening behavior seen at lower strain rates with the difference of maximum ~ 14% between calculated and experimental flow stress. It can be observed that the model can fairly predict the peak stress at both the strain rates. The difference in the calculated peak stress and experimental peak stress is maximum ~7% at both higher and lower strain rates.

Table 2: Parameters of the Hansel-Spittel equation

A	m_1	m_2	m_3	m_4	m_5	m_6
2136.313	-0.00243	0.2315	0.1215	0.0001	-0.001	0.3235

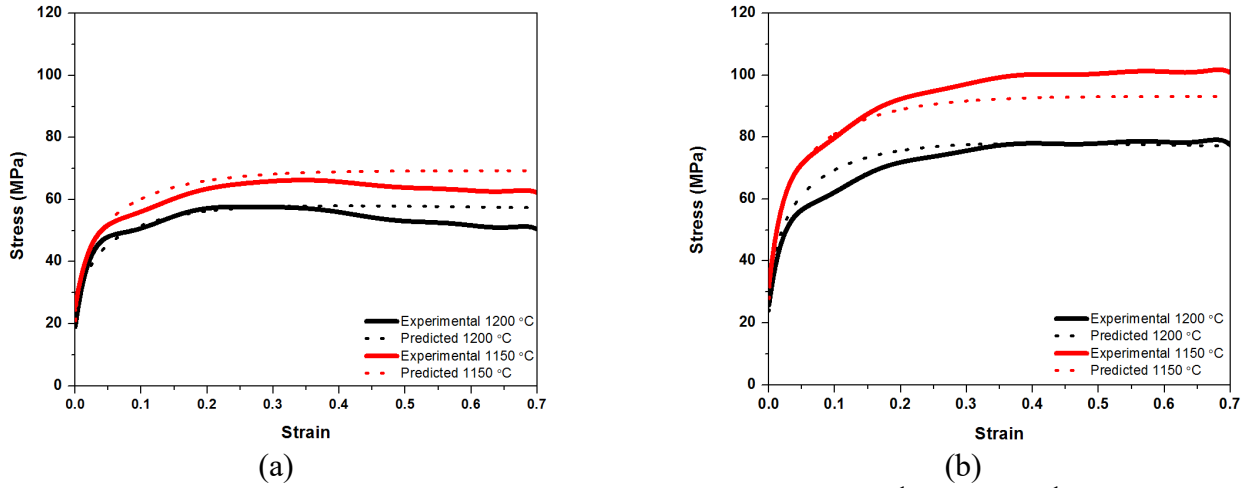


Fig. 1: Flow curves of 42CrMo at strain rate of (a) $0.25s^{-1}$ and (b) $2s^{-1}$.

Numerical simulation of 42CrMo hot forging

Numerical simulations generally consist of various elements which presents the real process. Among the various elements includes the geometrical models of ingot, dies, material model and a set of boundary and initial conditions. The die temperature was kept similar to the deformation temperature. The density of the alloy is $7386.80465 \text{ Kg/m}^3$ and specific heat is $661.94 \text{ J/Kg/}^\circ\text{K}$. Hansel spittel model was introduced in Forge NxT 1.0[®] software and two simulations at different strain rates, $0.25s^{-1}$ and $2s^{-1}$ at constant deformation temperature of 1200°C were conducted. The temperature distribution map for final stage of deformation for strain rate of $0.25s^{-1}$ and $2s^{-1}$ with deformation temperature 1200°C is shown in Fig 2. It is apparent from the Fig. 2 that temperature distribution in case of higher strain rate is more homogenous than at lower strain rate. Deformation heating is usually generated in any alloy during deformation and is the function of strain rate [1]. This heat generated is usually termed at adiabatic heating and causes higher heat in the sample thereby reducing the flow stress. Adiabatic heating is represented by the following equation:

$$\Delta T_{\text{Adiabatic}} = \frac{0.95 \int \sigma d\epsilon}{\rho C_p} \quad (2)$$

Where ΔT is the change in temperature, $\int \sigma d\epsilon$ is the area under the uncorrected stress- strain curve, ρ is the density, C_p the specific heat and 0.95 is the fraction of mechanical work transformed to heat with remaining fraction going to microstructural changes. Adiabatic heat calculated from the experimental data reveals that the temperature at the center at strain rate of $0.25s^{-1}$ and deformation temperature of 1200°C is 7.19°C at $0.25s^{-1}$ and 14.5°C at $2s^{-1}$. From the simulation results, the adiabatic heat generated due to hot compression at strain rate of $0.25s^{-1}$ and $2s^{-1}$ at a deformation temperature of 1200°C is $\sim 7^\circ\text{C}$ and $\sim 15^\circ\text{C}$. It is

also observed that temperature distribution along the sample after strain of 1 is not uniform at 0.25s^{-1} whereas it is significantly uniform at high strain (2s^{-1}). This temperature distribution reveals that Hansel-Spittel equation significantly predicts the adiabatic heat generated during the deformation at low and high strain rates in case of as-cast 42CrMo alloy.

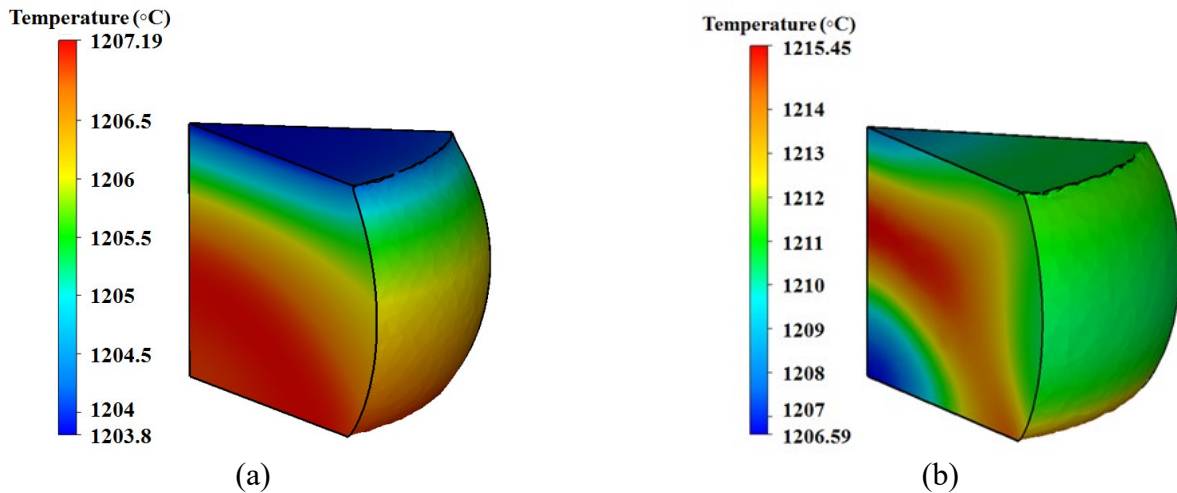


Fig. 2: Simulated temperature distribution map of 42CrMo at strain rate of (a) 0.25s^{-1} and (b) 2s^{-1} at deformation temperature of 1200°C .

To verify the accuracy this model further, force versus time analysis was compared. Fig. 3 shows the force versus time plot of predicted and experimental data. From the plots, it was found that at lower strain rates, Fig. 3 (a), the difference in predicted and experimental values is 17%, whereas at higher strain rate, Fig. 3 (b), the difference shoots up to 37%. The indifference in the force reading between the experimental and predicted result is mainly due to the effect of friction during hot compression. It is well known fact that friction plays a major role in stress strain plots during hot compression [12]. From the experimental values it was calculated that the friction effect was more at higher strain rates as compared to lower strain rates, which may have been the major cause of this deviation.

Conclusions:

1. Hot compression of as-cast 42CrMo alloy reveals that at low strain rates, dynamic recrystallization occurs whereas at low strain rates recovery occurs.
2. Hansel-Spittel equation fairly predicts the flow curves up to peak stress. However it is not able to predict softening of flow stress due to dynamic recrystallization.
3. Simulation results reveal that the model is able to predict the adiabatic heating during deformation, where as it is not able to predict the force with the time.

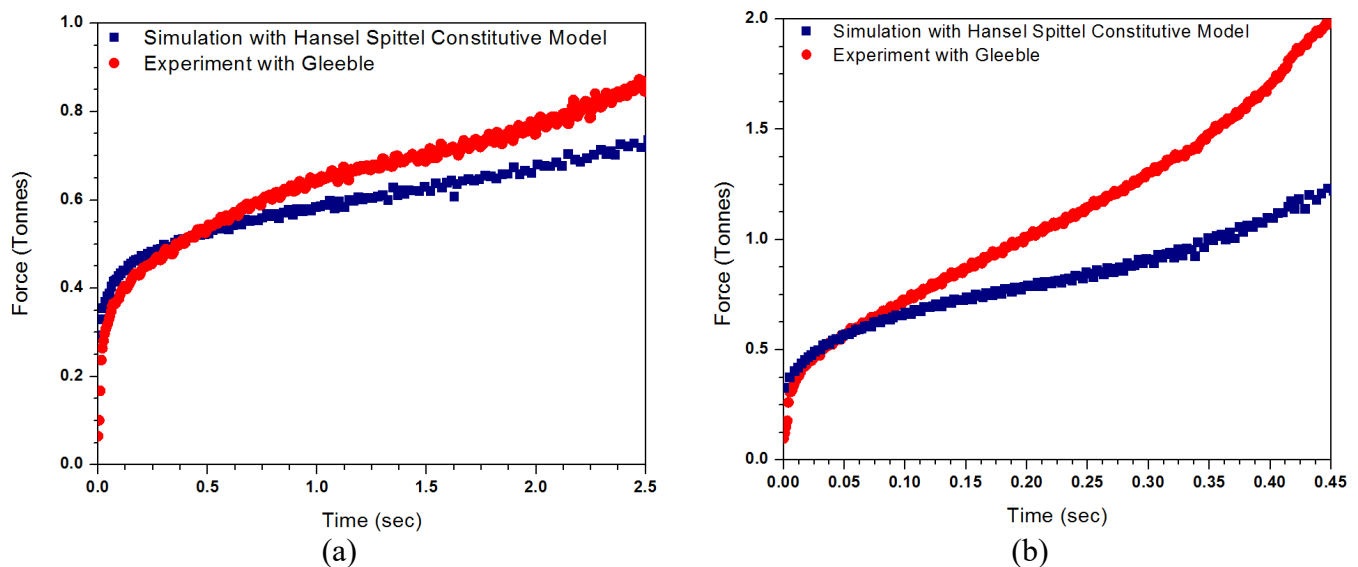


Fig. 3: Force versus time plot of experimental and predicted at strain rate (a) 0.25s^{-1} and (b) 2s^{-1} at deformation temperature of 1200°C .

Acknowledgements

The authors are very much grateful to Mr. R. Beauvais and Mr. R. Tremblay of Finkel Steel Co. for providing and machining the specimens for the present research. The authors are also grateful to NSERC for their financial support for this work.

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